Lawrence Berkeley National Laboratory - University of California

#### **ENGINEERING NOTE**

Author Department Date

James T. Goulding Mechanical Engineering 1/31/00

Cat. Code

**FE3313** 

Serial #

M7857

Page

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Program - Project - Job: SNS-FE Project

**MEBT Mechanical Systems** 

Title: SNS-FE MEBT 30mm & 40mm Beam Position Monitor Mechanical Design

#### 1. Scope

This engineering note describes the mechanical design for the 30mm Beam Position Monitor (BPM) and the 40mm Beam Position Monitor. It includes a drawing list of mechanical components and assemblies, design background, engineering calculations, outside vendor component information, and rendered pictures.

### 2. Drawings

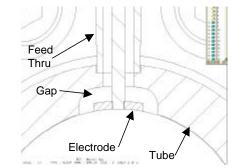
- 2.1. 25B170 30mm BPM Bellows
- 2.2. 25B171 BPM SMA Feed Thru
- 2.3. 25B172 40mm BPM Bellows
- 2.4. 25B173 30mm BPM Bore Tube
- 2.5. 25B174 30mm BPM Electrode Spool
- 2.6. 25B175 30mm BPM Bellows Seal Flange
- 2.7. 25B176 30mm BPM Fixed Flange
- 2.8. 25B177 30mm BPM Split Flange
- 2.9. 25B178 30mm Beam Position Monitor
- 2.10. 25B179 40mm BPM Fixed Flange
- 2.11. 25B180 40mm BPM Electrode Spool
- 2.12. 25B181 40mm BPM Split Flange
- 2.13. 25B182 40mm BPM Bellows Seal Flange
- 2.14. 25B183 40mm BPM Bore Tube
- 2.15. 25B184 40mm Beam Position Monitor

Copies of all drawings are included in the Appendix

### 3. Design Overview

The BPM is based on the design of a 20mm stripline beam position monitor (LANL drawing no. 144Y-618019) that was developed at Los Alamos National Laboratory for the ADT CCDTL. The

MEBT design differs from the LANL design in that machining the electrodes from a single spool of stainless steel. The base of the spool electrically shorts the electrodes together. The signal is taken from the free end through a microwave feed-through. The slots in the bore tubes (25B173 & 25B183) and the stripline tines on the electrode spool (25B174 & 25B180) were designed to maintain a  $50\Omega$  impedance. (For details of the electrical analysis, see SNS-Technical Note FE-EE-012.) The grounded stripline design



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requires half as many feed-throughs and should simplify assembly fixturing.

To maintain the  $50\Omega$  impedance, the geometry of the electrode, the slot and the gap between them had to be within a tolerance of  $\pm 5\%$  of nominal. The tolerance stack and tolerance sizing calculations are shown in the Appendix. Design issues included sizing the bellows, and having clearance for the mounting hardware.

#### 4. Reference

- 4.1. CCDTL BPM Segment 6/7 20mm Bore, Drawing No. 114Y618019 (Los Alamos National Laboratory)
- 4.2. CCDTL BPM Segment 107/108 25mm Bore, Drawing No. 114Y618050 (Los Alamos National Laboratory)
- 4.3. Ultra-High Vacuum Microwave Feed-Through, SMA Female (Spec Sheet), Kaman Instrumentation Publication SMA-1000-3/95. (Copy of spec sheet included in Appendix.)
- 4.4. Contour Plot of Electrostatic Potential (included in the Appendix).
- 4.5. SNS Technical Note FE-EE-012, Basic Electrical Design of the MEBT BPM
- 4.6. Engineering Calculation Notes (included in appendix).
- 4.7. Standard Bellows Company homepage: www.std-bellows.com

#### 5. Fabrication and Assembly Issues

Most of the component fabrication can be done with conventional milling and turning operations. However, the following features will be done using wire EDM:

- Bore tube inside diameter
- Bore tube slots on inside diameter
- Spool inside diameter
- Spool electrode tines

The wire EDM allows for better precision on the tighter profile callouts. It also allows for better thin wall cuts.

Because of the design, it is extremely difficult to make internal welds. External welding is far more practical. To help minimize the problem of virtual leaks caused by external welds, all fabricated components are ultra-high vacuum cleaned and electropolished before being welded into the assembly. Since they will be sitting on the shelf for months after assembly, another cleaning (water based) may be required. The vacuum in the beam pipe will in the 10<sup>-6</sup> to 10<sup>-8</sup> torrs range.

The feed-throughs are connected to the electrode tines to maintain electrical contact. The electrode is made of 316 stainless steel and the feed-through conductor is made of TZM (see spec sheet in Appendix D). Because the melting point of TZM is so high compared to 316 stainless steel, these two materials are not well suited for TIG welding. Torch brazing is a potential method, however there is a worry that the heat involved could cause the TZM to crystallize and crack. Another route is soldering. This would require the connection point on each component to be pre-tinned then assembled and heated to make the connection.

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### 6. SNS-FE Personnel

Daryl Oshatz, MEBT Lead Mechanical Engineer James T. Goulding, Mechanical Engineer Larry Doolittle, Electrical Engineer

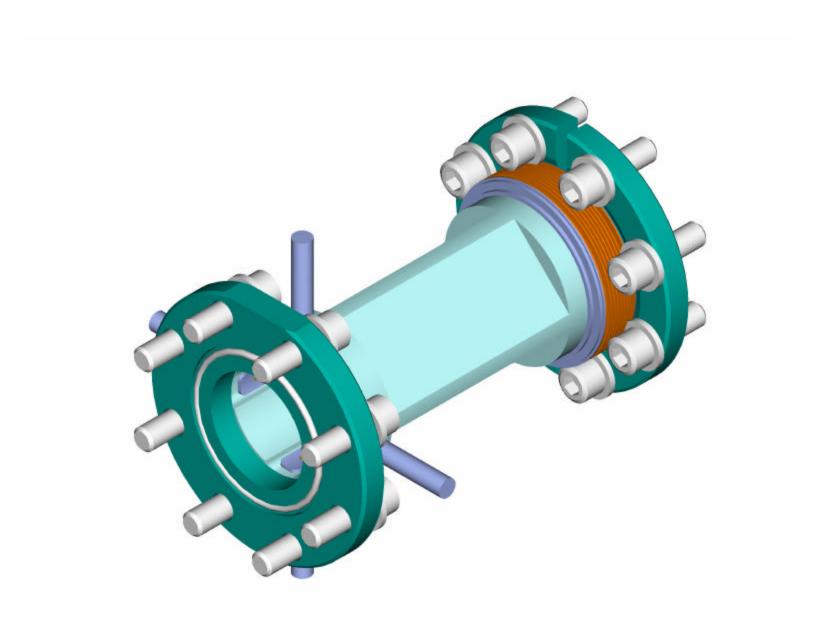
### 6. Appendices

Appendix A: Rendered Pictures of 3-D CAD model Appendix B: Component and Assembly Drawings Appendix C: Engineering Calculations and Plots

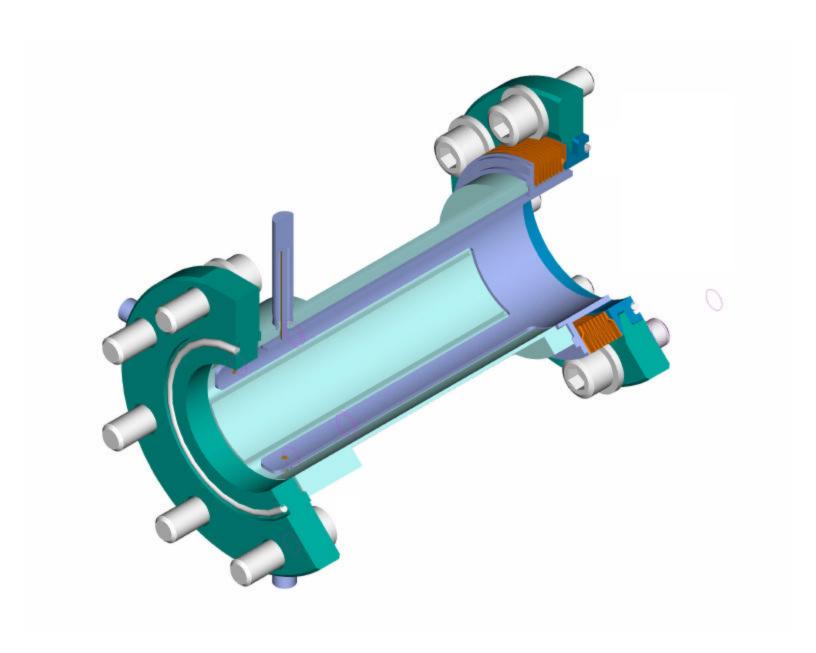
Appendix D: Vendor Specification Sheets

# Appendix A

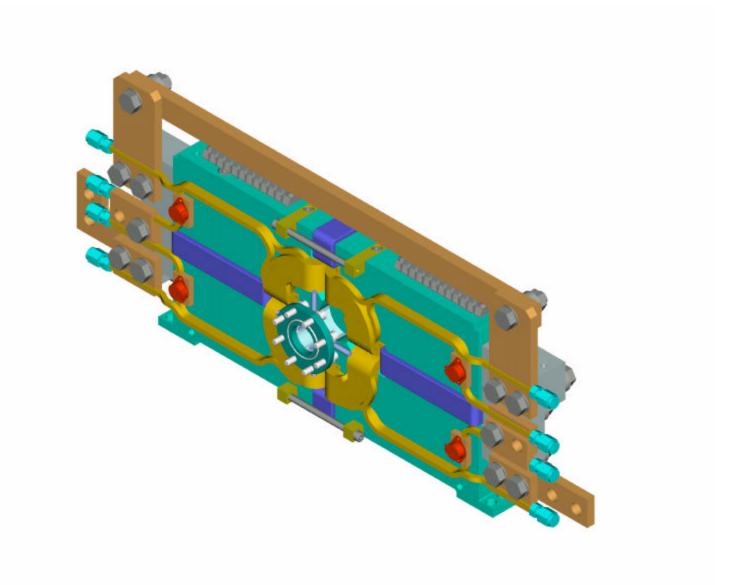
# 30 mm Beam Position Monitor



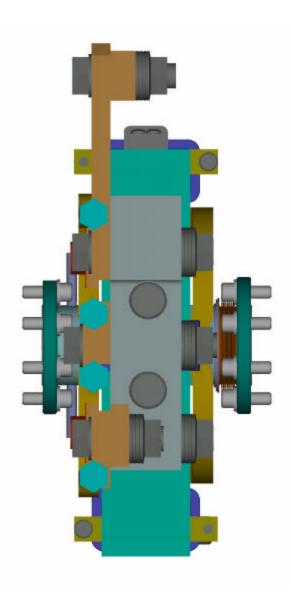
# 30mm BPM Cross Section View

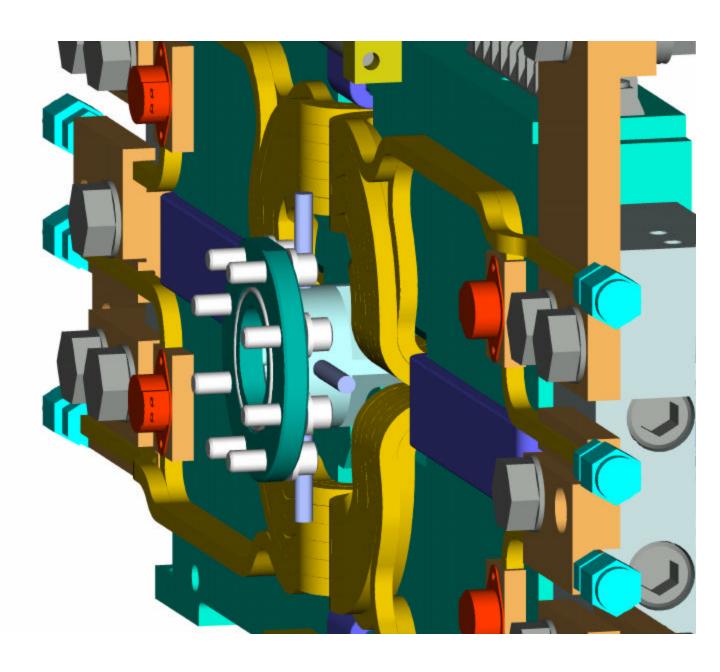


# 32mm Quadrupole Magnet with 30mm Beam Postion Monitor

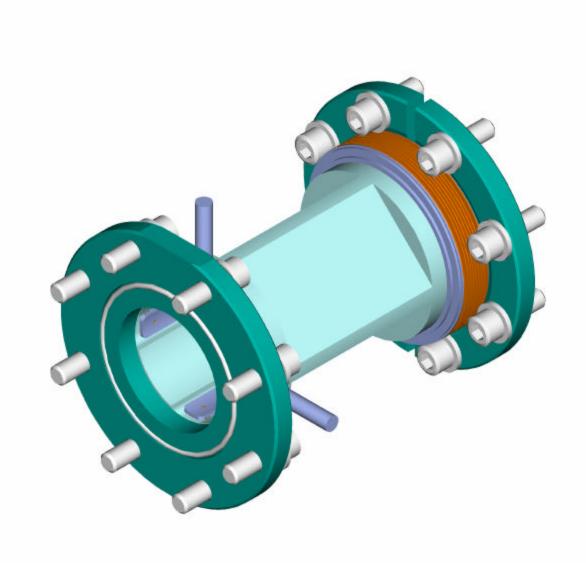


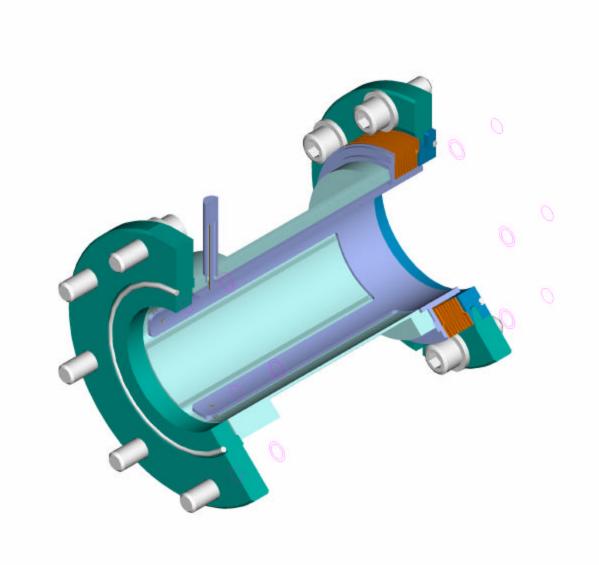
# 32mm Quadrupole Magnet with 30mm Beam Postion Monitor



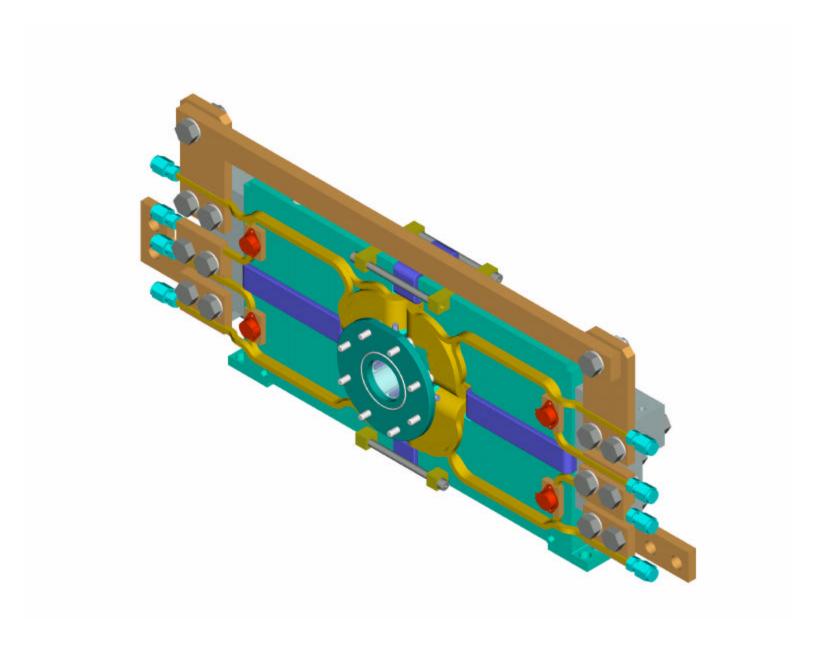


# 40 mm Beam Position Monitor

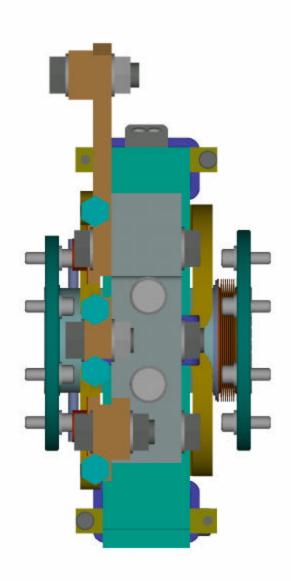




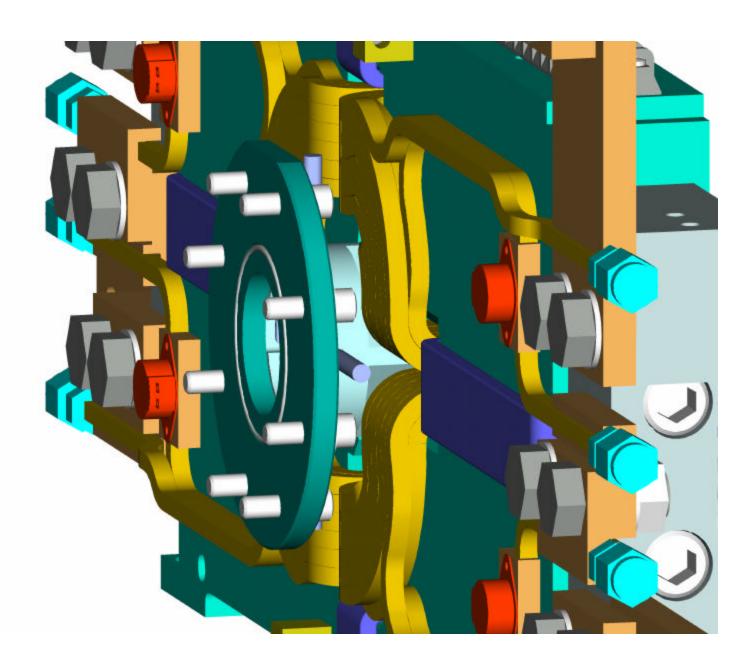
# 42mm Quadrupole Magnet with 40mm Beam Postion Monitor



# 42mm Quadrupole Magnet with 40mm Beam Postion Monitor

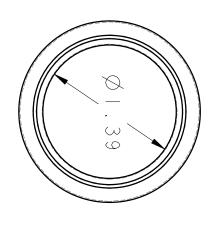


# 42mm Quadrupole Magnet with 40mm Beam Postion Monitor



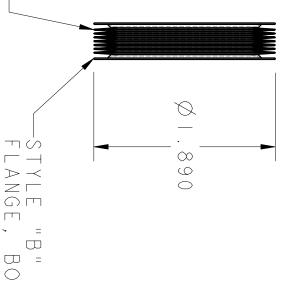
# Appendix B

STANDARD BELLOWS P/N: 189-139-1/2-B DRAWING FOR PRICING QUOTATION ONLY. \* \* 89 in 25BI70 \_ B



89-139 BELLOWS-1/2 SEGMENT.

BOTH SIDES



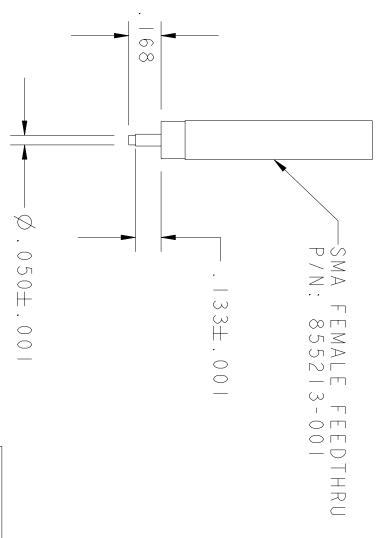
Remove Burrs, Weld Splatter & Loose Scale  $x\pm 0.1 \times x\pm 0.01 \times xxx\pm 0.005 \times x \times \pm 0.5$ In Accordance With ASME Y14.5N 1994 & B46.1 Break Edges .016 Max on Machined Work Unless Otherwise Noted Date Date Date Regd Deliver Finish 347 STAINLESS STEEL | B | - | 1/25/00 | ADDED INFORMATION TO TITLE BLOCK Do Not Scale Prints Scale 1/1 Rev Dwn Date Changes LAWRENCE BERKELEY NATIONAL LABORATORY | Shorm on 25B178 | Dwg. No. | Size | University of California - Berkeley MECHANICAL SUBSYSTEMS 30 MM BPM BELLOWS Code FE3313 SNS-FES MEBI SHEET 1 OF 1 Size Rev

Drawing: BPM\_30\_BELLOWS Type: PART Model: BPM\_30\_BELLOWS

25B171 1B

FEMALE

NOTES
1. ULTRA-HIGH VACUUM MICROWAVE FEED-THROUGH, SMA
2. DRAWING FOR PRICING QUOTATION ONLY.



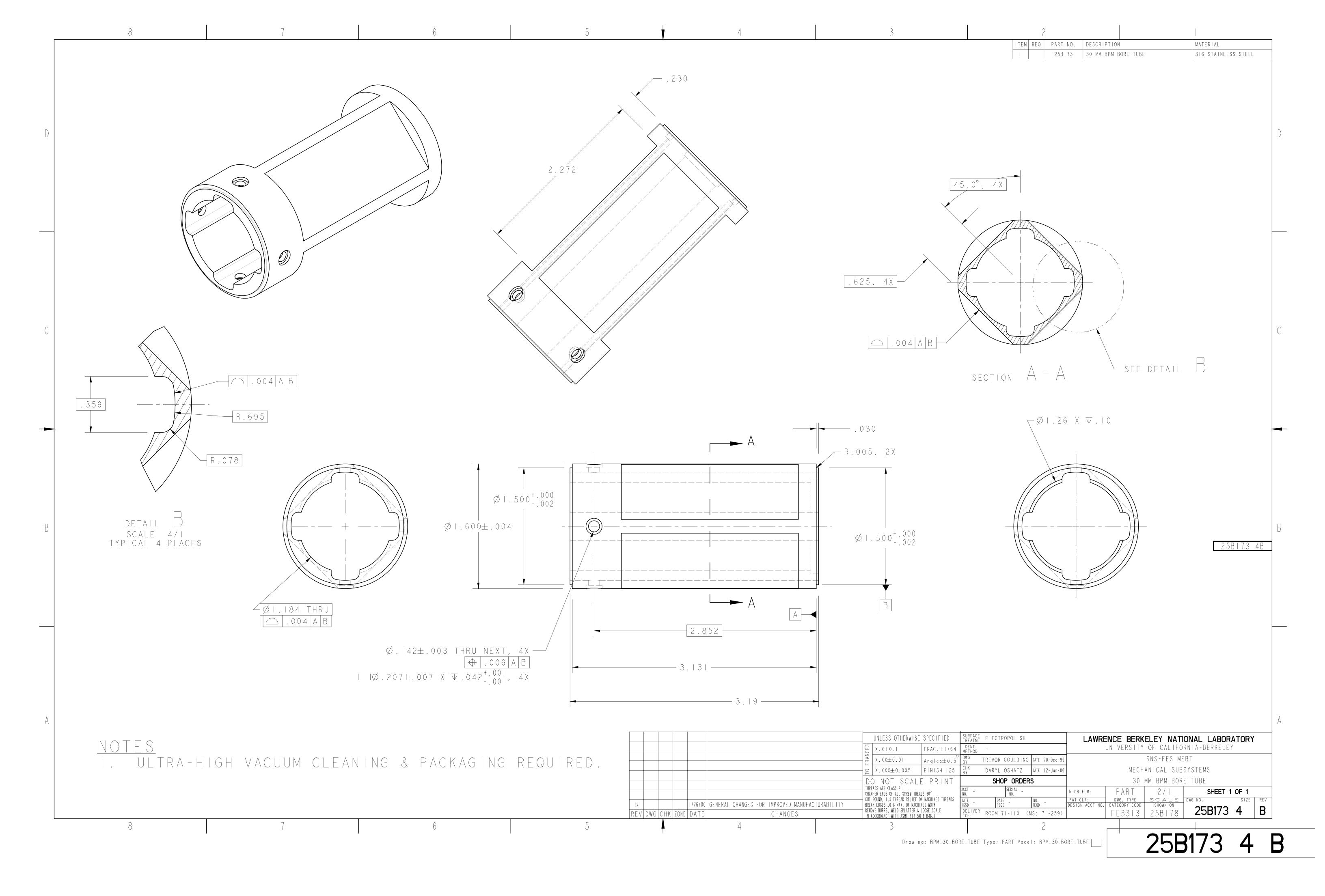


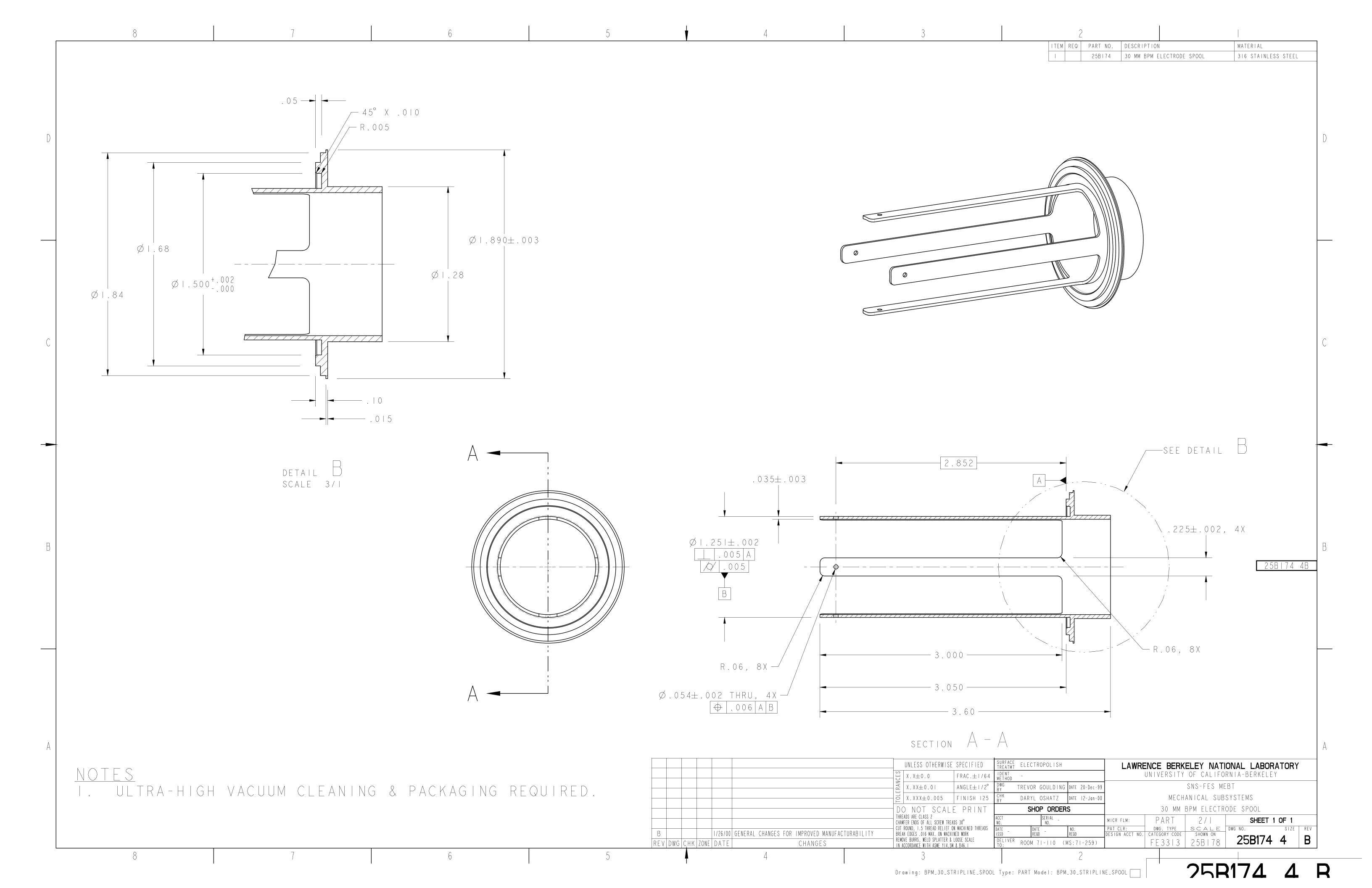
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By TREVOR GOULDING Date	17-Dec-99	Filmed -	Dwg No. 25B178, 25B184 Dwg. No.	Dwg No. Size Rev
Check DARYL OSHATZ Date	I - JAN - 00	Design Account XXXX	Account XXXX-XX   Drawing PART   258171	25B171 1 B

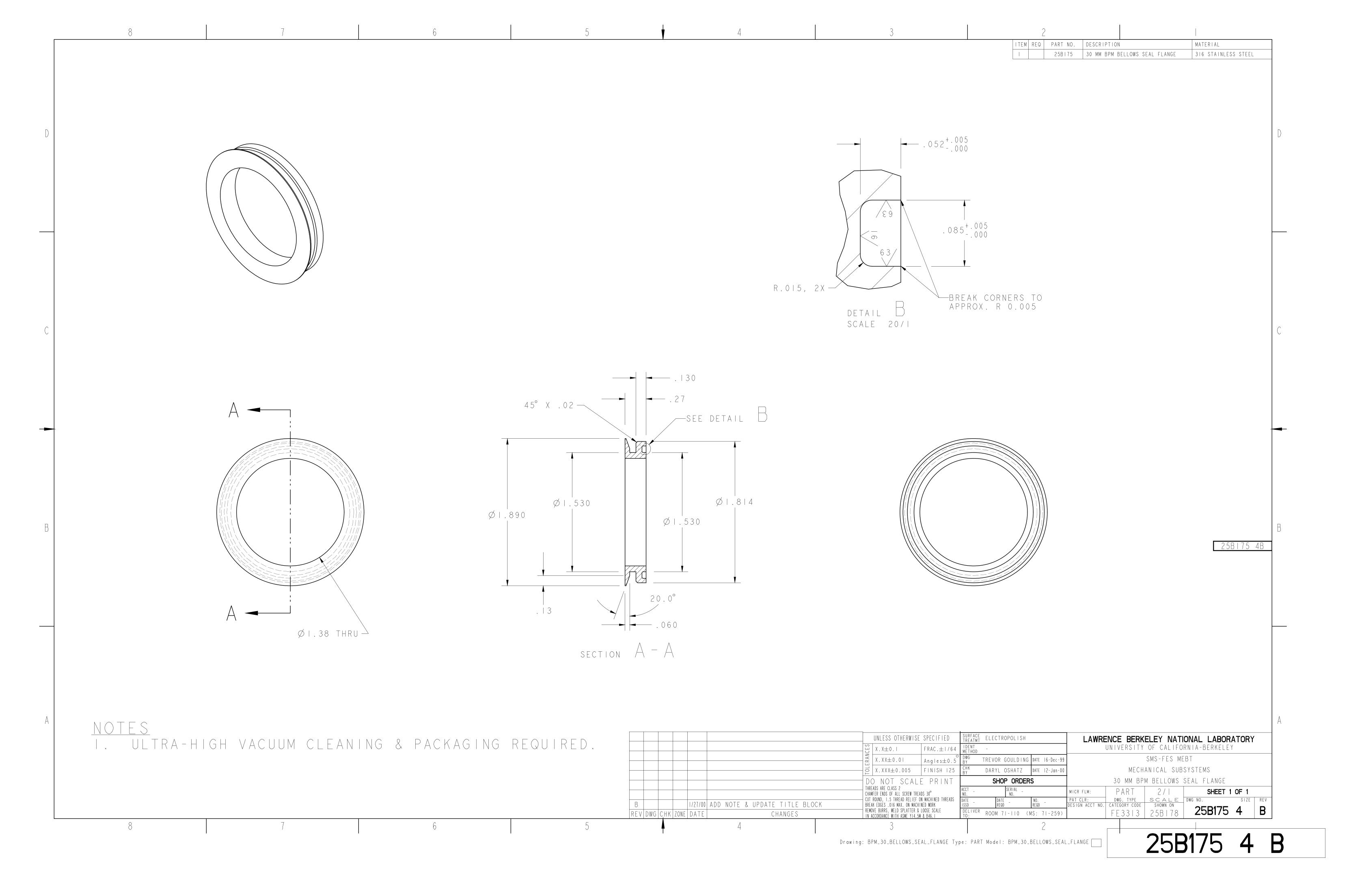
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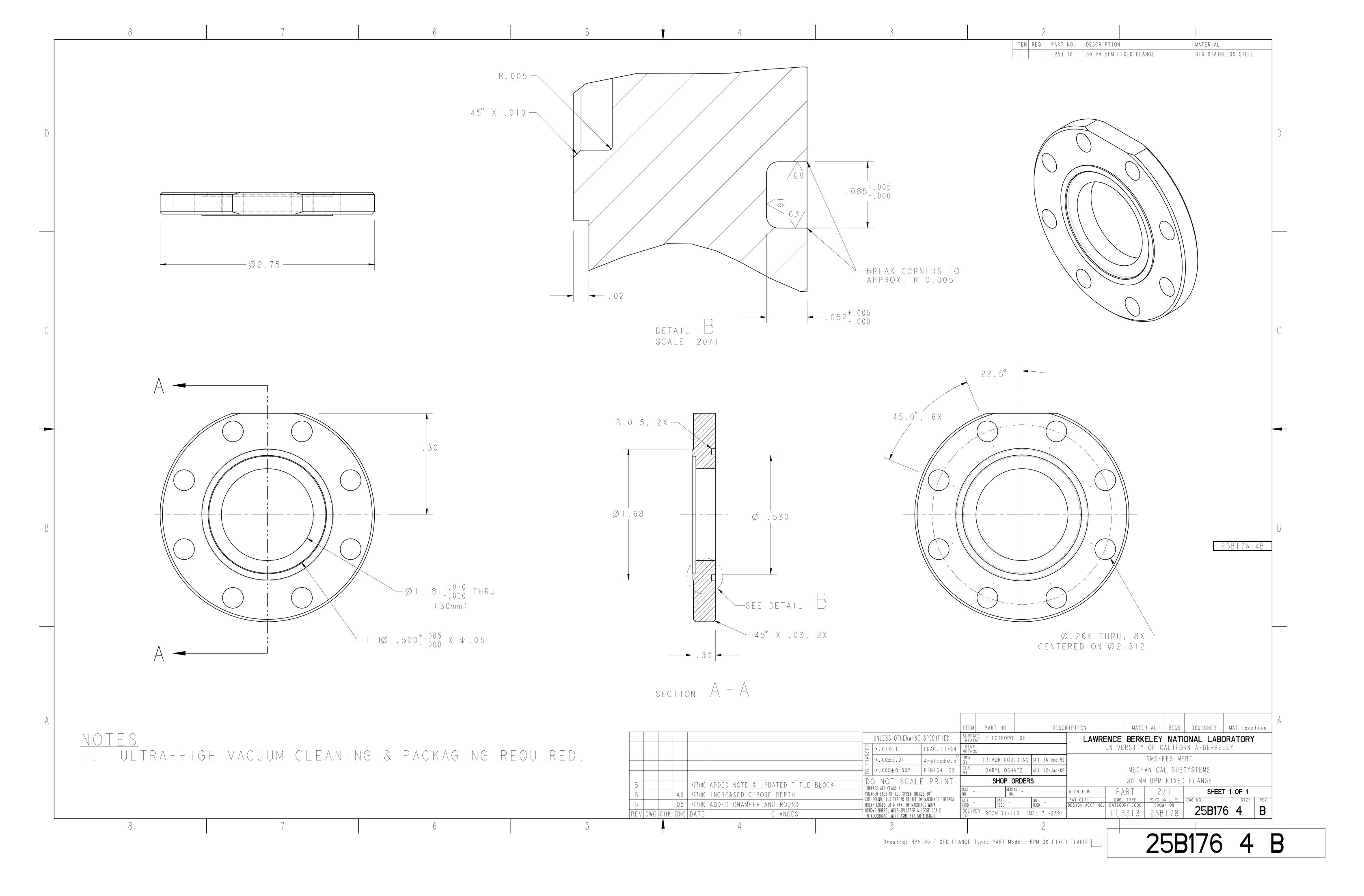
STANDARD BELLOWS P/N: 250-175-1/2-B DRAWING FOR PRICING QUOTATION ONLY. SEGMENT. Material Remove Burrs, Weld Splatter & Loose Scale x±0.||.xx±0.01||.xxx±0.005|| x.x°±0.5 In Accordance With ASME Y14.5N 1994 & B46.1 Break Edges .016 Max on Machined Work Drawing: BPM\_40\_BELLOWS Type: PART Model: BPM\_40\_BELLOWS TREVOR GOULDING Date

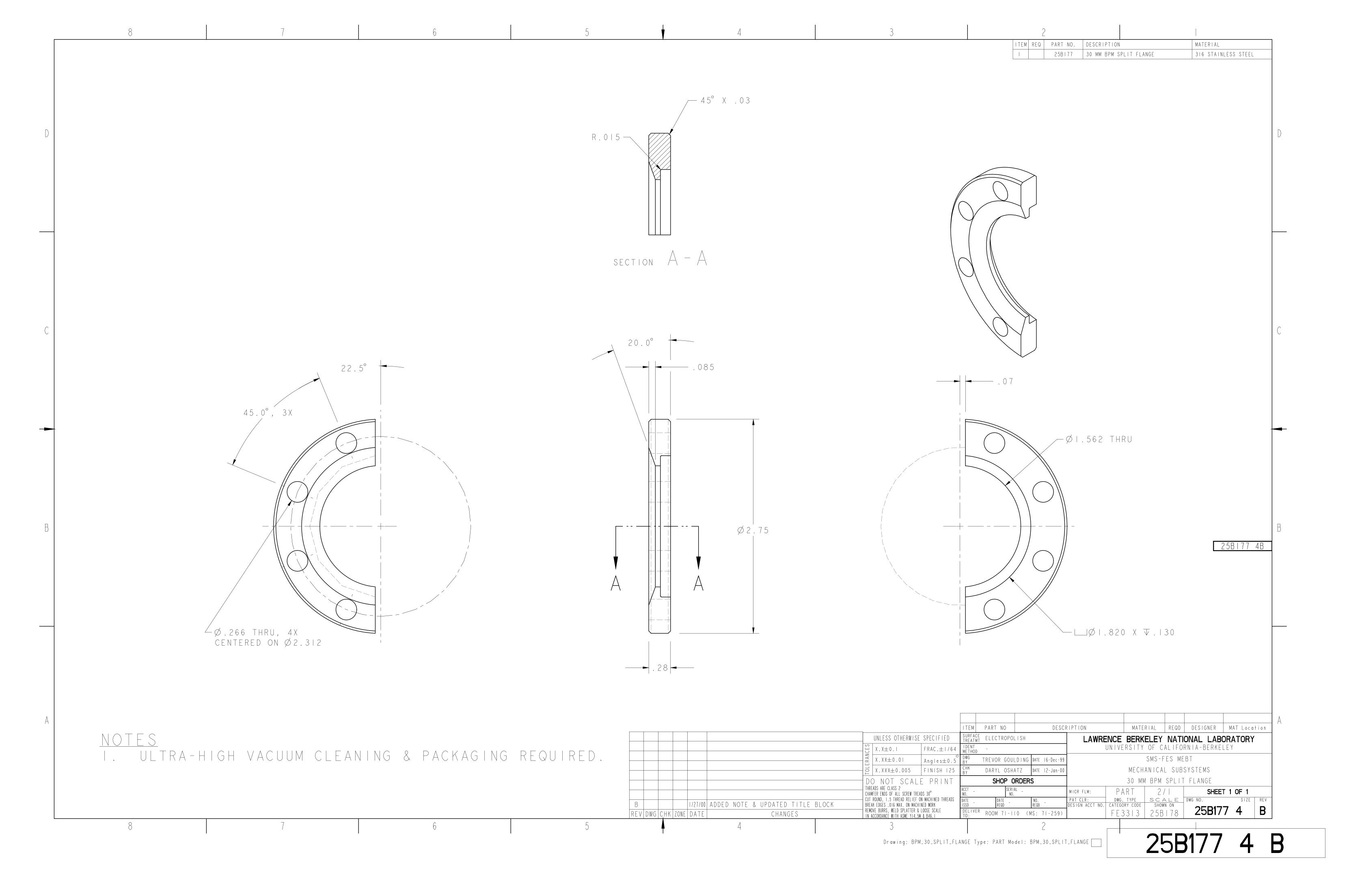
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- Sharmon 25B184 Dwg. No. Size
XXXX-XX Procing PART 25B172 1 University of California - Berkeley MECHANICAL SUBSYSTEMS 40 MM BPM BELLOWS SNS-FES MEBI BOTH SIDES 25BI72 Size Rev \_ B

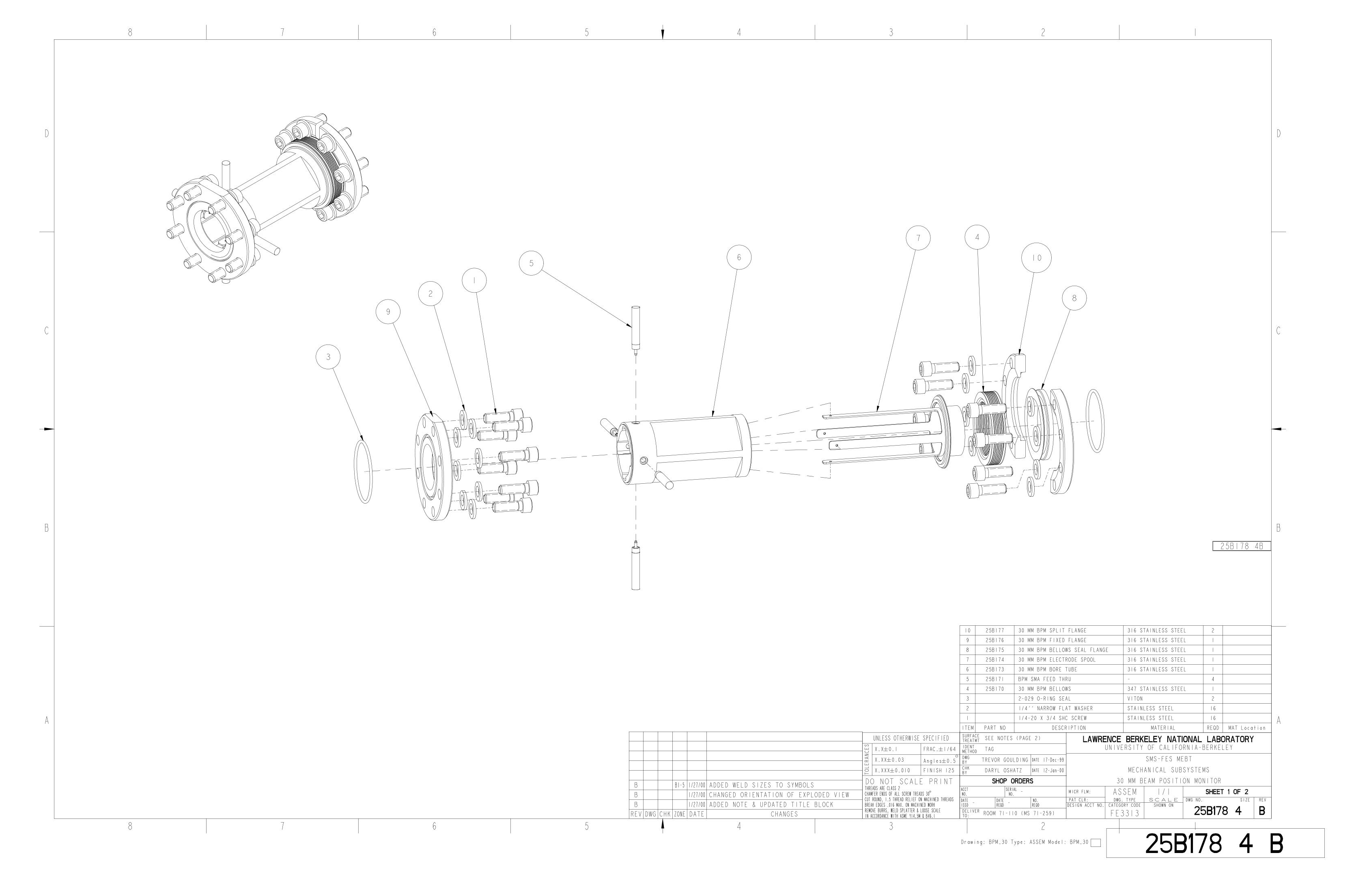


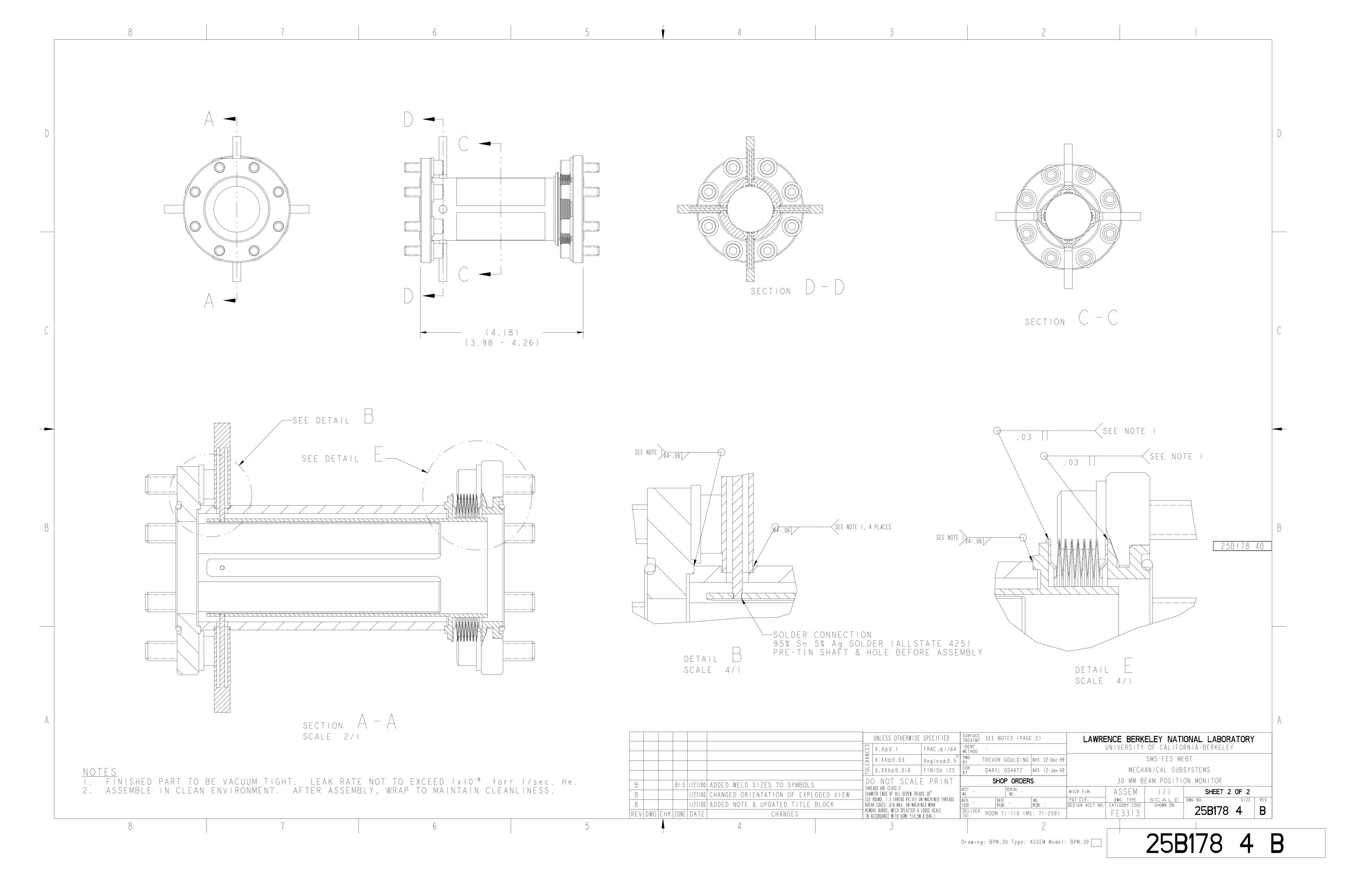


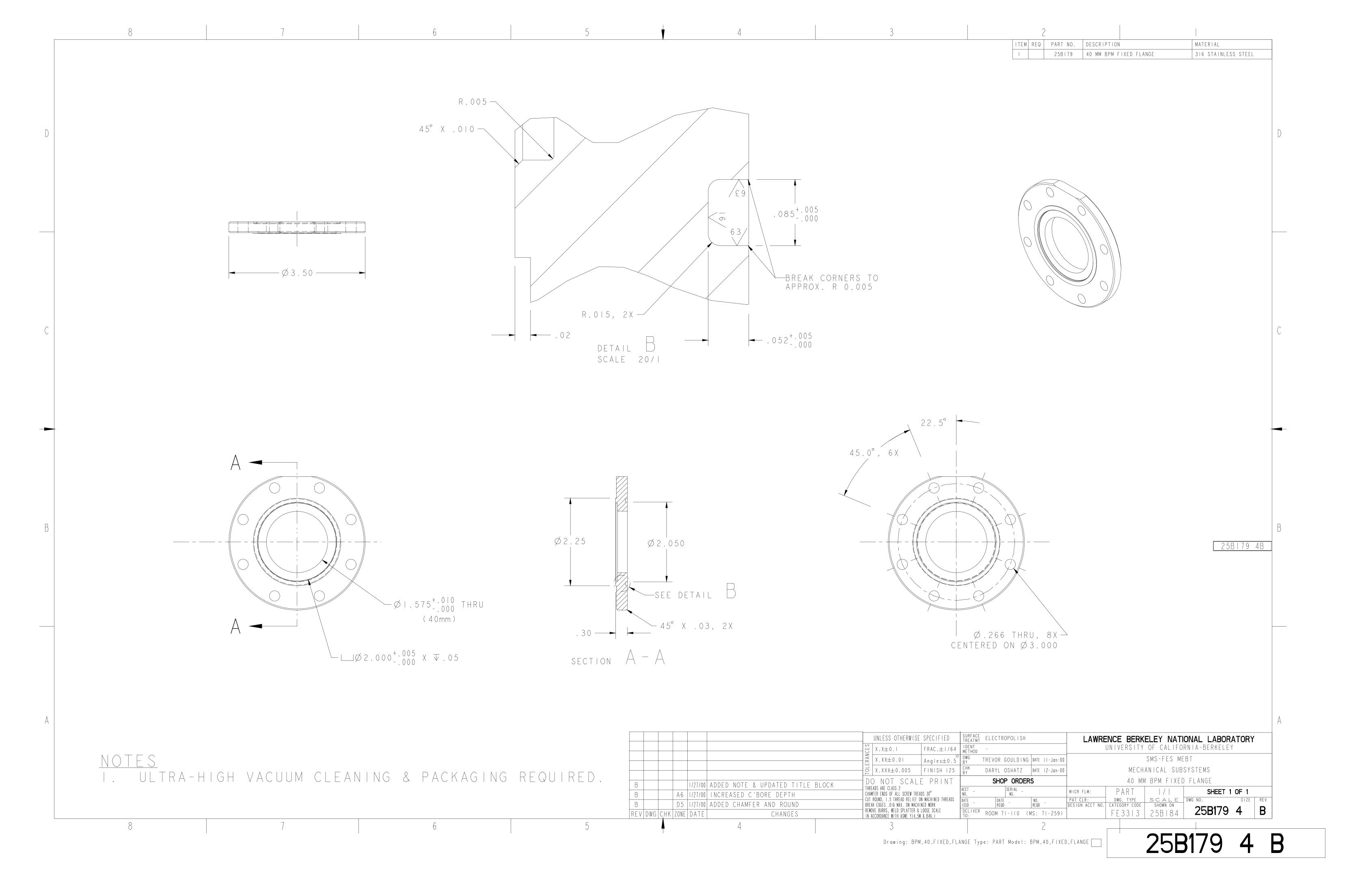


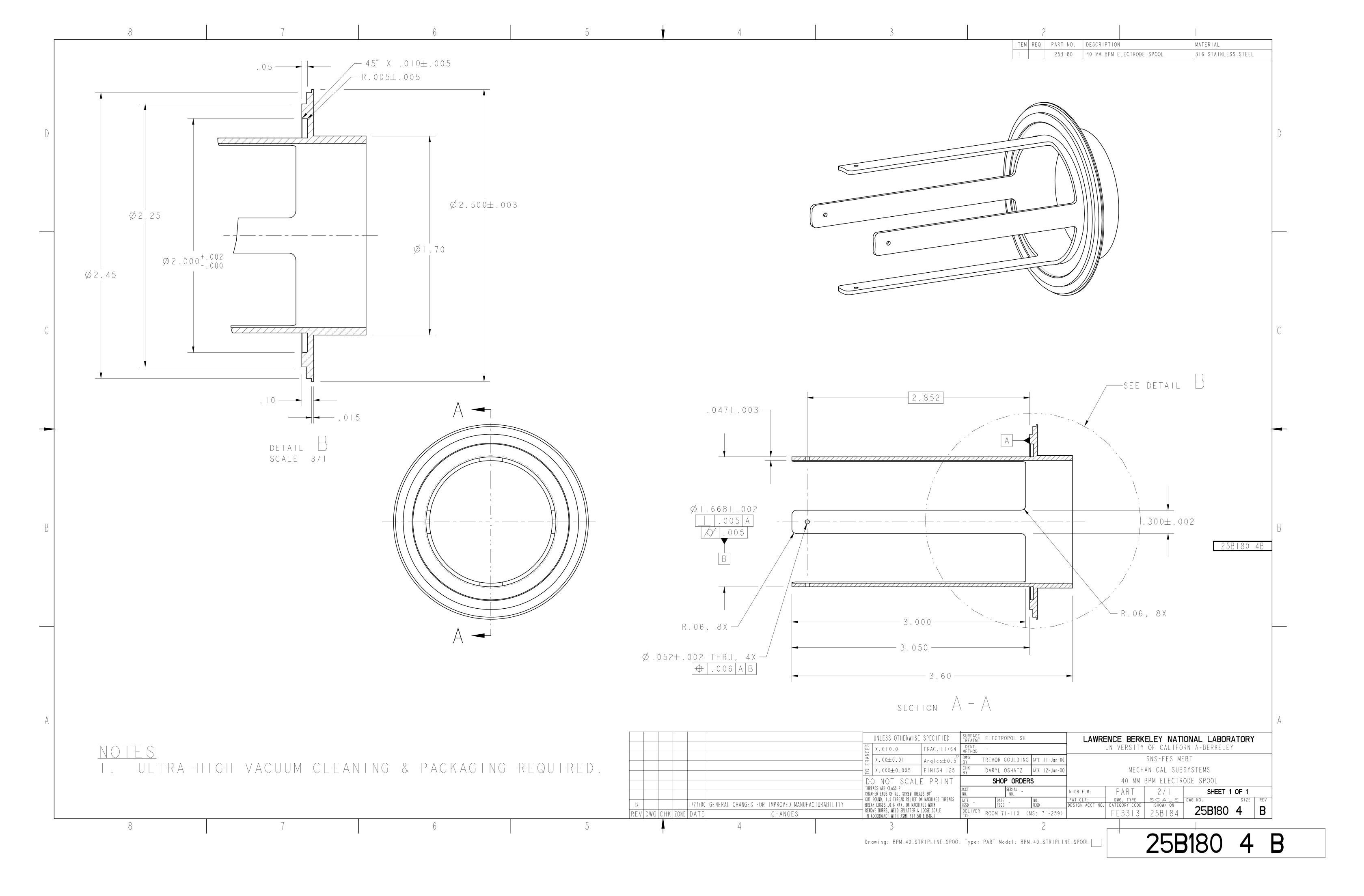


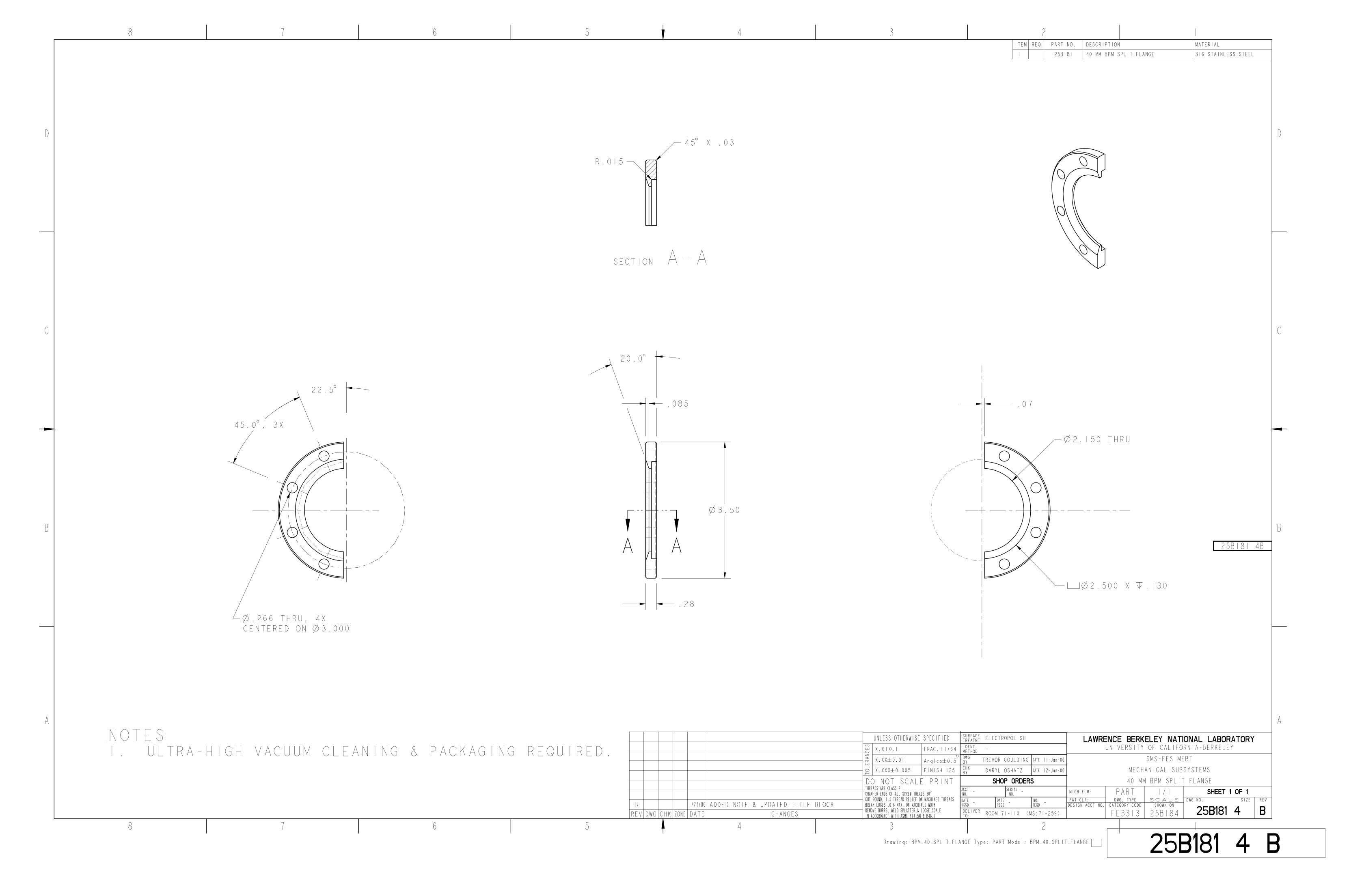


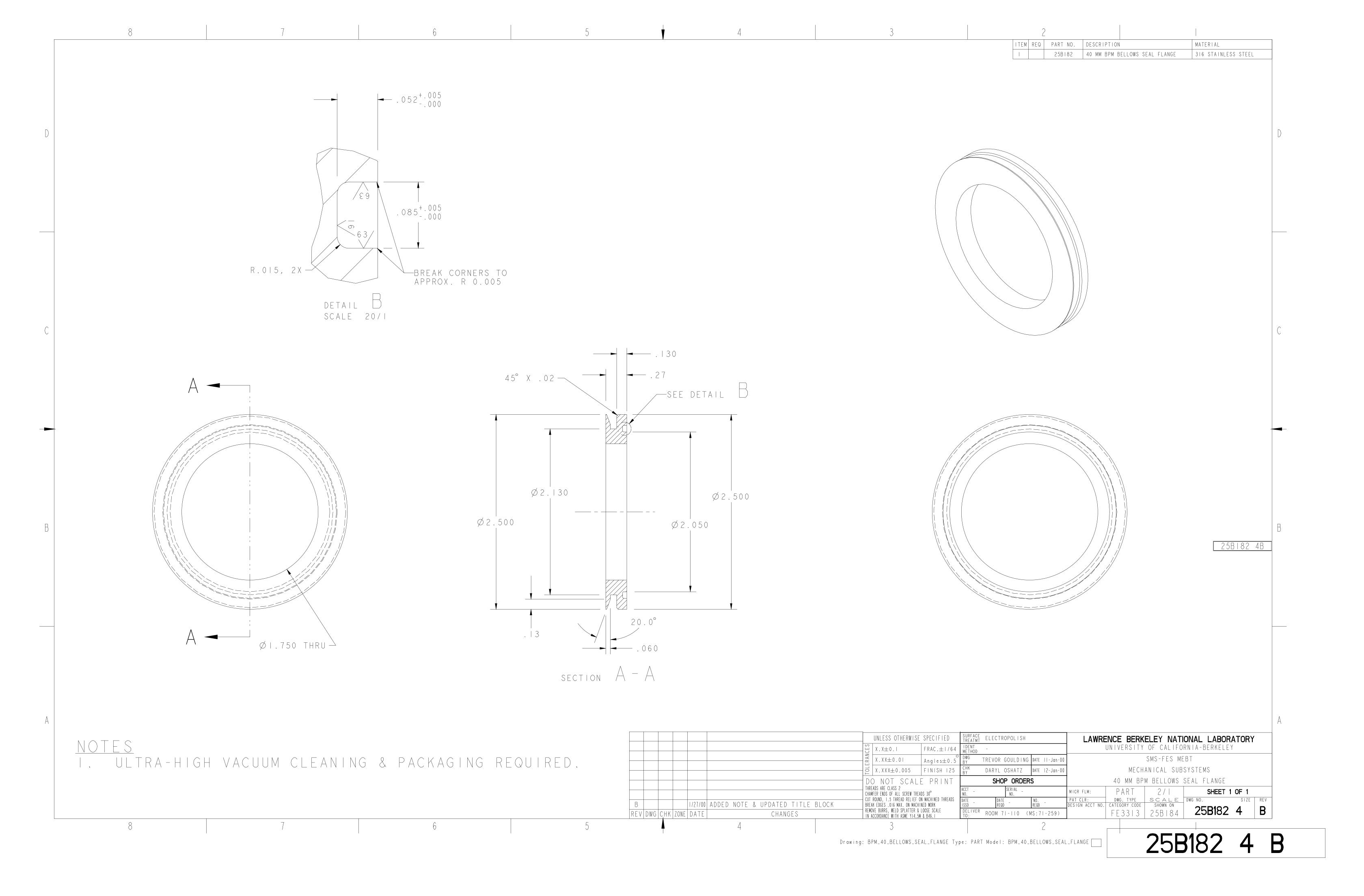


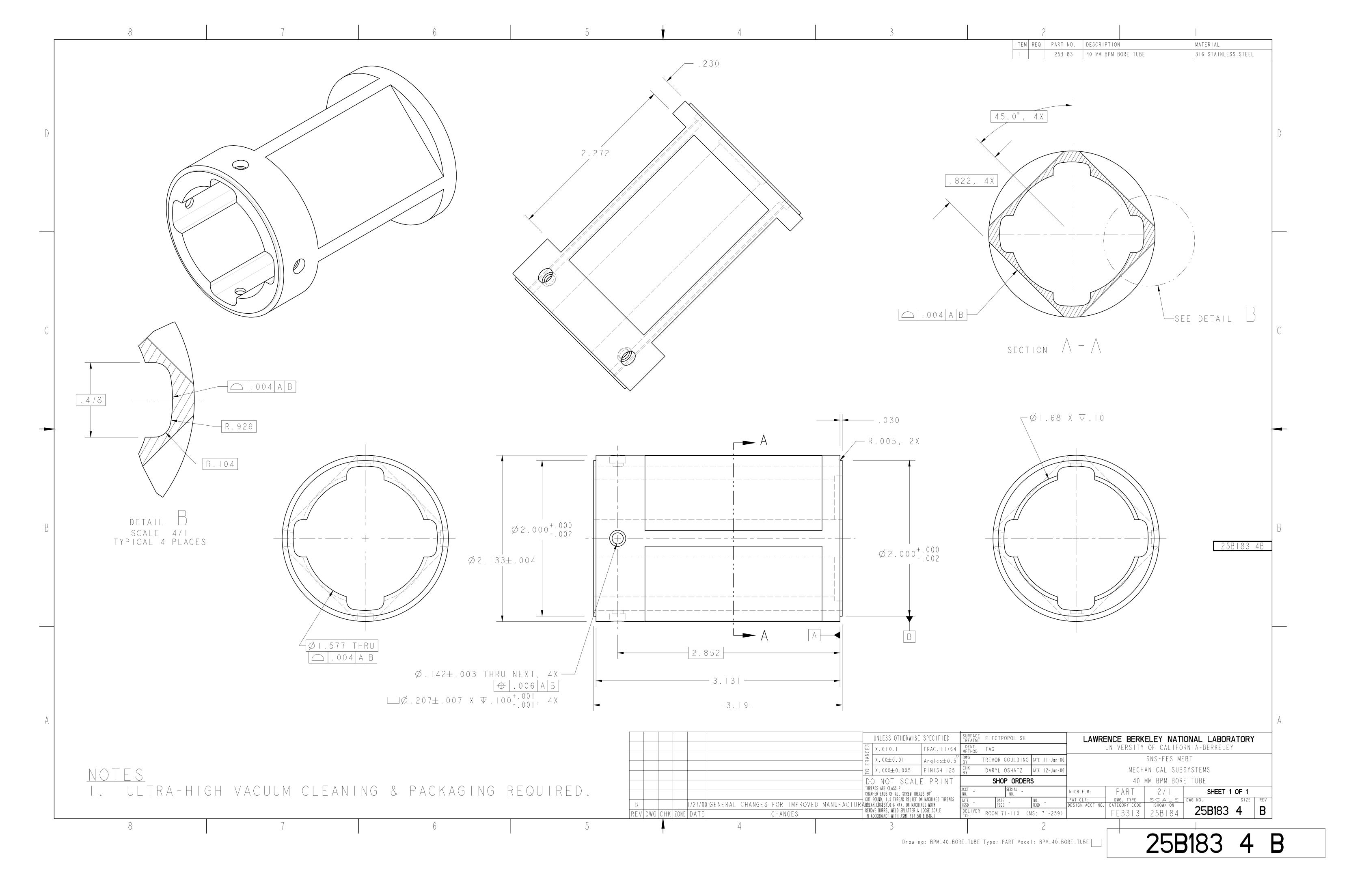


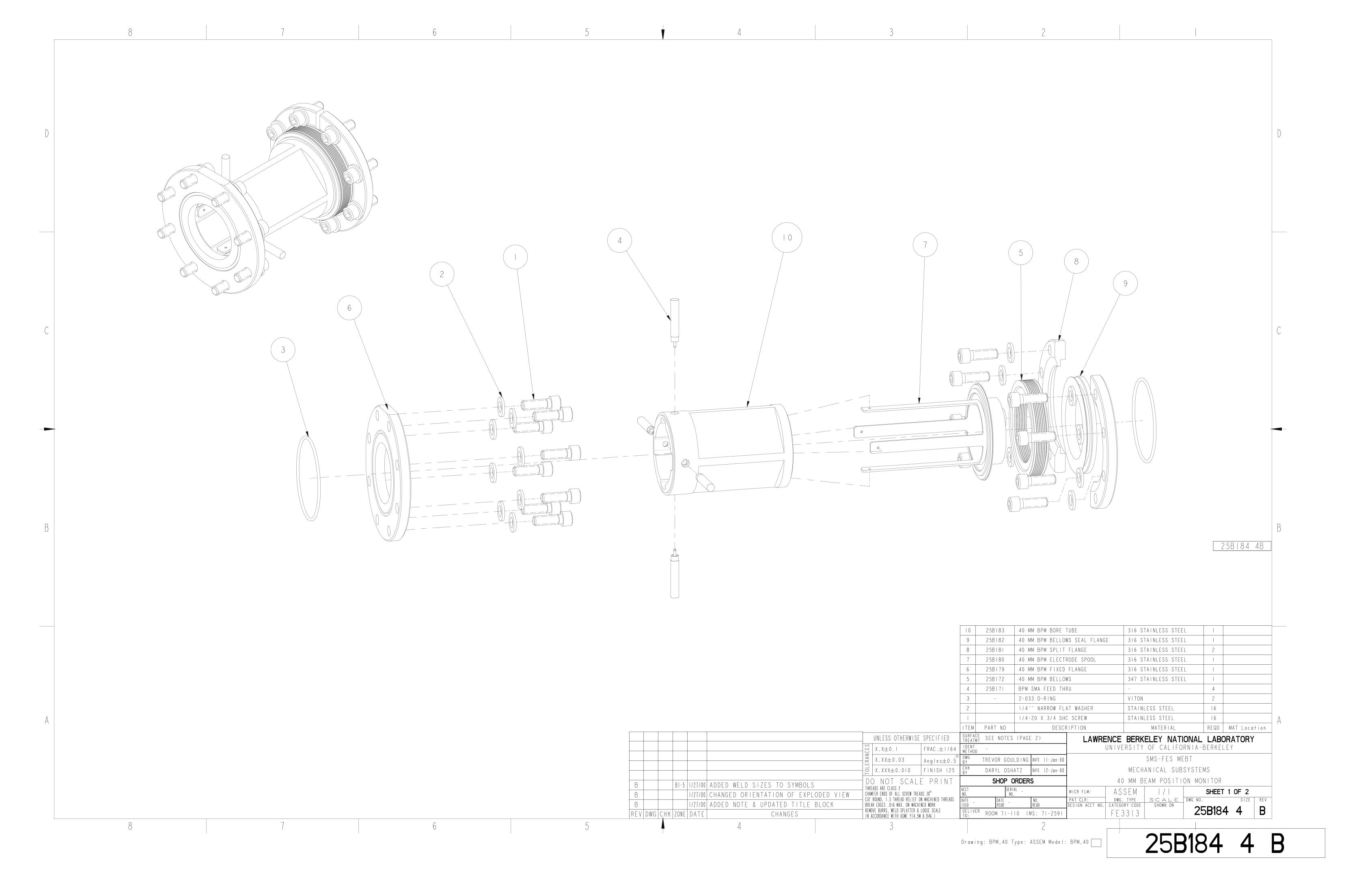


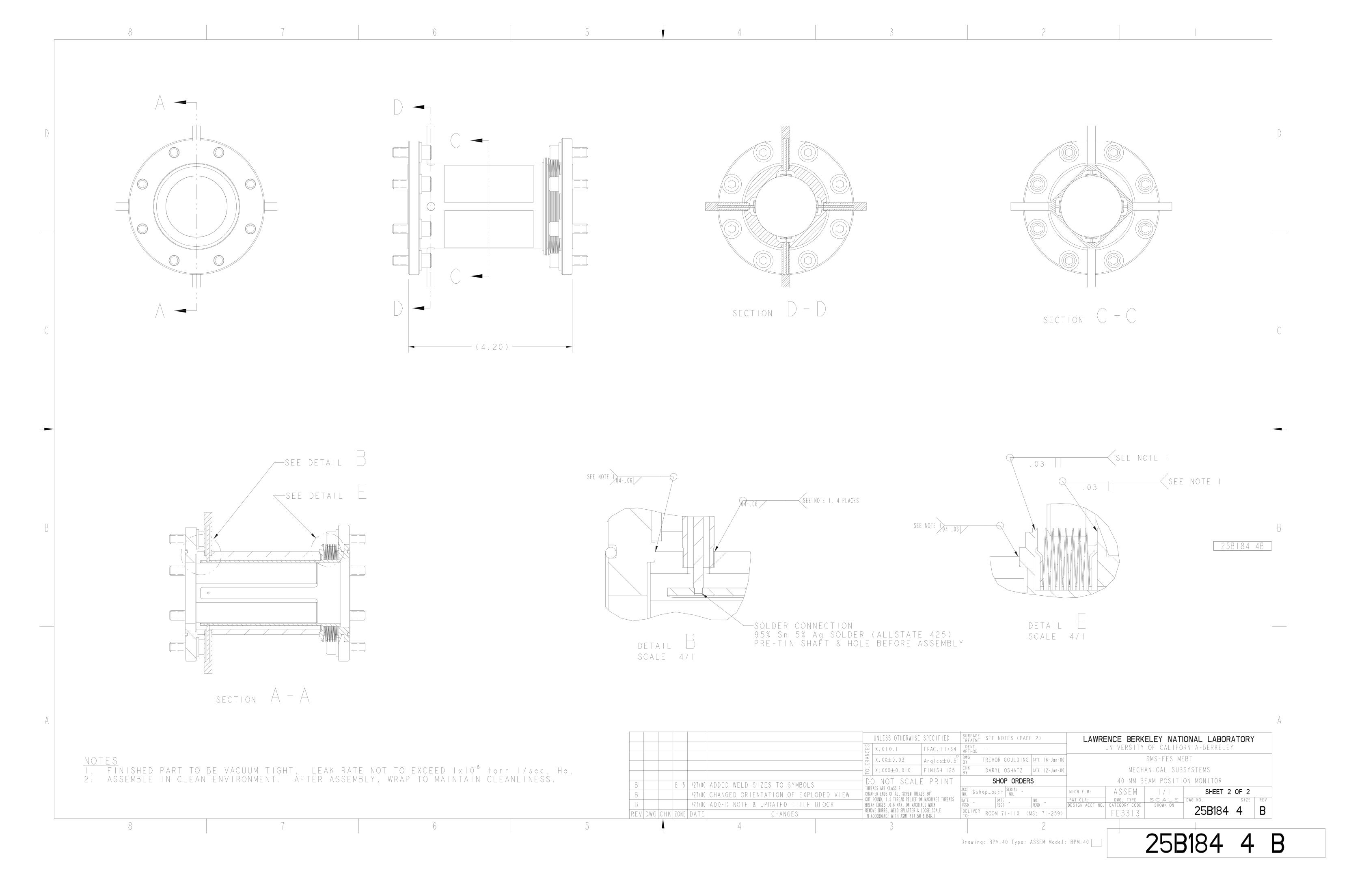












# Appendix C

TOLERANCE STACK UP ANALYSIS

## ASSUMPTIONS:

- STAN WITHIN 5% OF NOMINAL FER RECOMMENDATION OF LARRY DOBLITTLE. (SEE
- 2. RSS (ROOT SUM SQUARED) METHOD WILL BE USED FOR ALL TOLERANCE STACK UP ANALYSIS

## ELECTRODE AND SIDT GEOMETRY DIMENSION MAINTAIN SOIR

HOT TO SCALE

RESISTANCE (PROVIDED BY LARRY DOUTTLE)

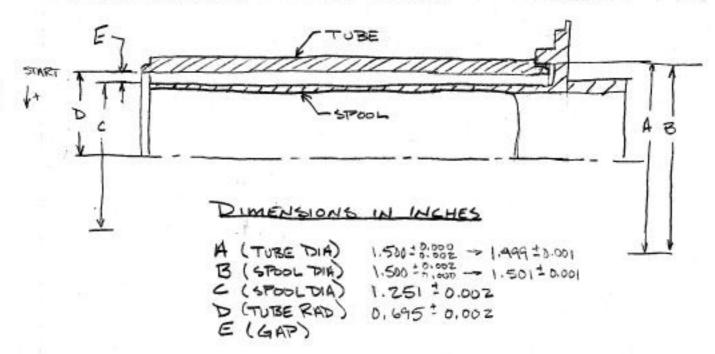
DIMENSIONS IN MM.

A - 15.00 B - 0.889 C - 1.761 2.862 1,703 1.993

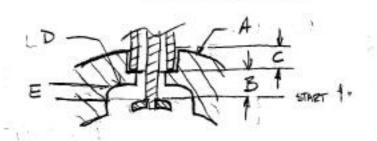
DIMENSION C IS CRITICAL AT \$5% OF NOMINAL

1.761 = 0.088 - 0.069 = 0.0035 in

TOLERANCE STACKS MUST BE ± ± 0.003 in -



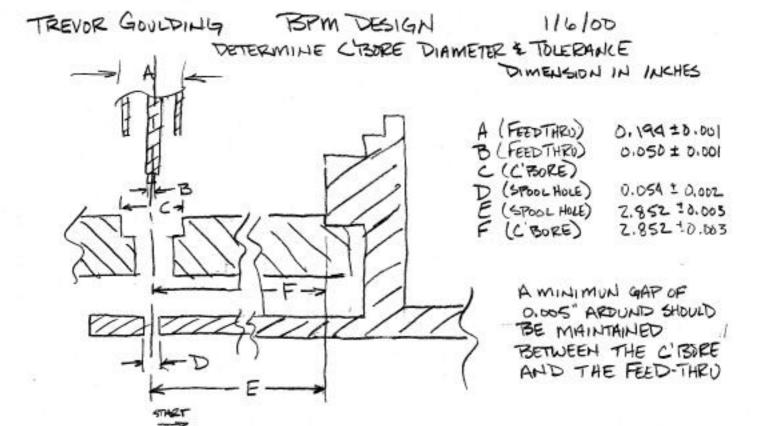
E = 0.070 +0.003



### DIMENSIONS IN INCHES

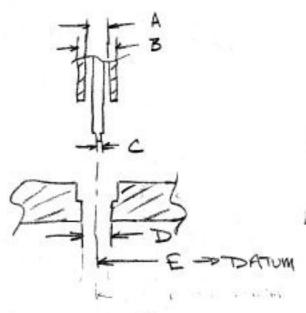
A (TUBE 0.D.) 1600 ± 0.004
B (FEEDTHRU COND) 0.133 ± 0.001
C (C'BORE) 0.042 ± 0.001
D (TUBE SLOT RAD) 0.695 ± 0.002
E (GAP)

E = 0.070 + 0.003



C = 0: 184 = 0.207 = 0.007

# TREVOR GOULDING BPM DESIGN 1/19/00 DETERMINE THAT L'BORE WILL ADEQUATELY SEAT FEED THRU



### DIMENSIONS IN INCHES

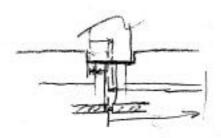
A (FEEDTHRU) 0.14Z ± 0.001
B (FEEDTHRU) 0.194 ± 0.001
C (FEEDTHRU) 0.050 ± 0.001
D (TUBE HOLE) 0.14Z ± 0.003
E (TUBE HOLE) 7.95Z ± 0.003
F (SPOOL HOLE) 0.054 ± 0.002
G (SPOOL HOLE) 7.85Z ± 0.003
H (GAP)



## FEED THRU WALL THAKKNES

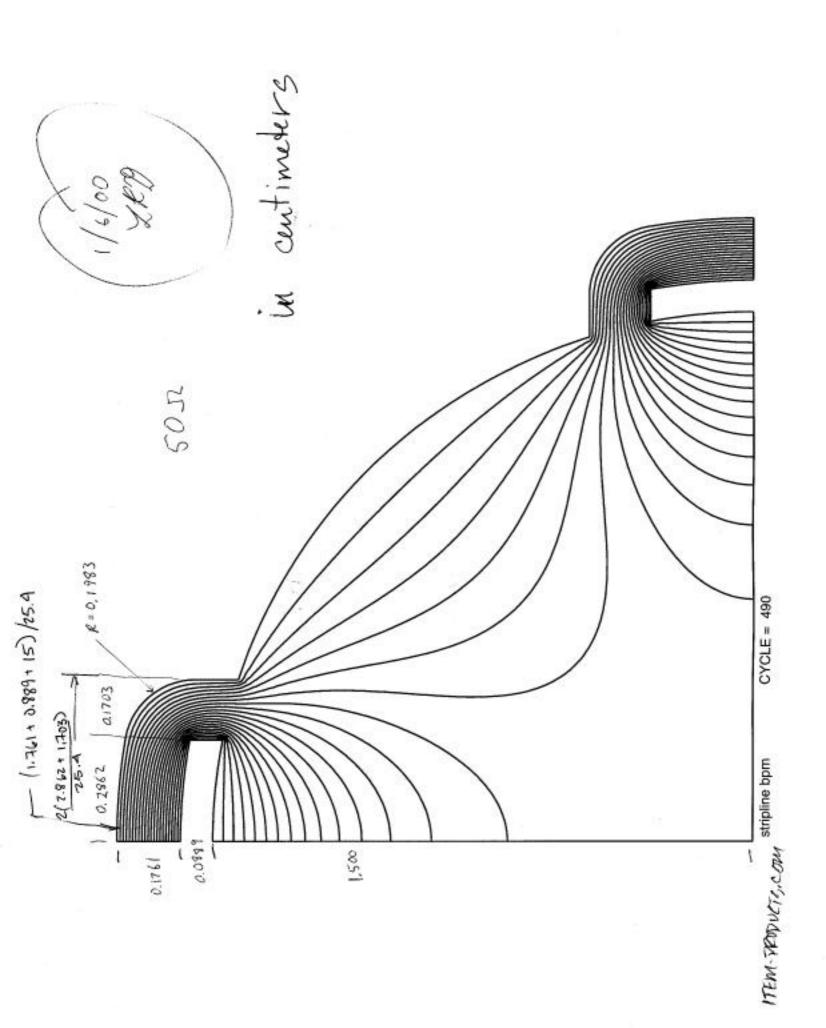
WALLMIN = 1/2 (Ammi - Bmax) = 1/2 (0.193-0.193)

= 0.025



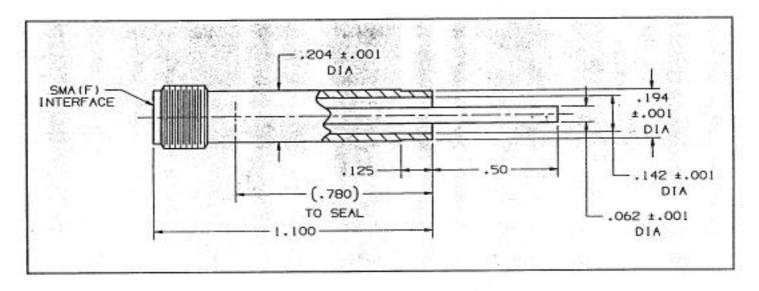
## WORST CASE ENGAGEMENT

H= 1/2 Bmin + 1/2 Cmin - 1/2 Fmax + Gmin - Emax - 1/2 Dmax = (1/2) 0.193 + (1/2) 0.009 - 1/2 (0.056) + 2.849 - 2.855 - (1/2) 0.195 = 0.015



# Appendix D

# ULTRA-HIGH VACUUM MICROWAVE FEED-THROUGH, SMA FEMALE



### S P E C I F I C A T I O N S

Impedance: 50 ohms.

Frequency range; DC to 20 GHz.

VSWR: 1.03:1 max to 3 GHz;

1.15:1 max to 20 GHz.

Insertion loss: 0.10 dB max @ 3 GHz.;

0.50 dB max @ 20 GHz.

Insulation resistance: >1012 ohms.

Voltage: 1,500 VRMS.

Operating temperature range:

Based on outer body material -

304 stainless steel: 77°K to 573°K

(-196°C to +300°C).

316 stainless steel: 4°K to 573°K

(-269°C to +300°C).

Inconel\*: 77°K to 773°K (-196°C to +500°C).

Hermeticity: <1x10<sup>-11</sup> cc He/sec.

Radiation: >200 megarads gamma.

Connector interface: SMA per MIL-C-39012.

#### Materials:

Outer body: 304 stainless steel, 316L stainless

steel, or Inconel\*.

Center conductor: TZM molybdenum per

ASTM B365.

Insulator: AL20, strengthened boro-silicate seal

(130,000 psi compressive strength).

Connector contact: Gold-plated BeCu.

Weldability: Laser, e-beam, TIG.

Custom materials: Cupronickel, monel, and

titanium.



MICROWAVE PRODUCTS GROUP

#### A FORTUNE 500 COMPANY

1500 Garden of the Gods Road Colorado Springs, Colorado 80907 Telephone 719/599-1821 Fax 719/599-1823